

A SIMPLE EMPIRICAL NOISE MODEL OF SUBMICRON-GATE GaAs MESFET FOR CAD APPLICATIONS

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Abstract

A simple empirical noise model of GaAs MESFETs with submicron gate is presented. From noise parameter measurements on various types of GaAs MESFETs, the intrinsic noise current sources have been found to be represented in simple empirical equations. Hence the noise parameters can be determined only from its small-signal equivalent circuit, and a good agreement is obtained between the model and measurement. The model presented here does not require additional noise measurement, and is suitable especially for microwave CAD applications.

Introduction

GaAs MESFETs are widely used for low-noise applications in microwave and millimeter-wave frequencies. Their noise properties are characterized by the noise parameters; the minimum noise figure F_{min} , the effective noise resistance R_n and the optimum source reflection coefficient Γ_{opt} .

The noise parameters of GaAs MESFETs are determined by experimental measurement [1]-[3], or by theoretical analysis based on physical model [4], [5], or by empirical model [6]-[11]. Among these, an empirical noise model, if applicable to a wide range of device geometry and operation, would be most preferable, since it provides an efficient and economical means of noise parameter calculation for computer-aided design (CAD) of microwave integrated circuits (MICs) and monolithic MICs (MMICs).

In this paper, a simple empirical noise model of submicron-gate GaAs MESFETs is described. While the previously reported empirical models [8]-[11] require noise measurement in addition to the small-signal equivalent circuit of FETs, the model presented here enables to calculate the noise parameters only from the small-signal equivalent circuit.

Noise Model of GaAs MESFETs

The noise model of GaAs MESFETs can be described by using a small-signal equivalent circuit and noise sources as shown in Fig. 1. The noise due to each parasitic resistance is the thermal noise associated with each resistance at ambient temperature T_0 , and is given by

$$\langle v_r \cdot v_r^* \rangle = 4 k T_0 B R_p \quad (1)$$

where v_r denotes the thermal noise voltage generated in the resistance R_p , $\langle \rangle$ a statistical average, $*$ the complex conjugate, and k is the Boltzmann's constant, B the bandwidth. On the other hand, the noise of intrinsic FET is related with two partially correlated noise current sources, i_g and i_d , having the following relations [4];

$$\langle i_g \cdot i_g^* \rangle = 4 k T_0 B G_{gn} \quad (2)$$

$$\langle i_d \cdot i_d^* \rangle = 4 k T_0 B G_{dn} \quad (3)$$

$$\langle i_g \cdot i_d^* \rangle = 4 k T_0 B (jC(G_{gn} G_{dn})^{1/2}) \quad (4)$$

where G_{gn} is the gate noise conductance, G_{dn} the drain noise conductance, C the correlation coefficient of i_g and i_d , and $j^2 = -1$.

Using (1)-(4), noise parameters can be calculated easily by the method in [12].

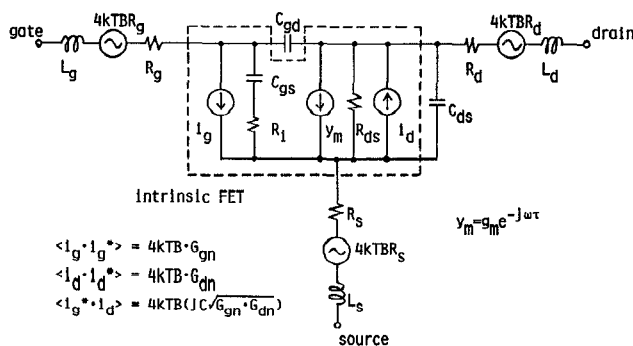


Fig. 1 Noise model of GaAs MESFET.

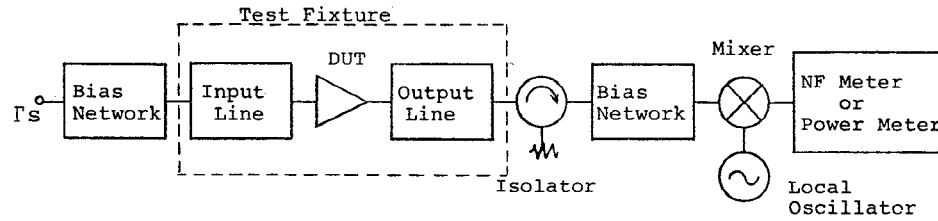


Fig. 2 Diagram of noise parameter measuring system.

Experimental Measurement

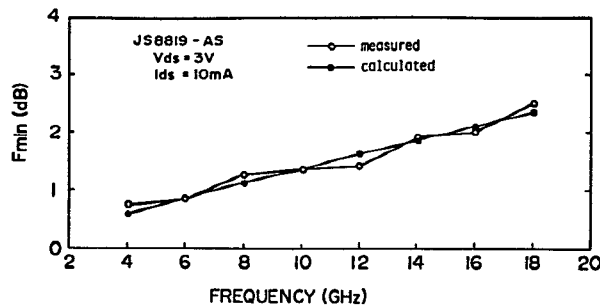
In order to determine G_{gn} , G_{dn} and C , noise parameters and S-parameters have been measured on various types of GaAs MESFETs.

Noise parameter measurement has been done over 4-18 GHz by using the modified method in [3]. Noise parameters have been obtained from the dependence of the output noise power on the source reflection coefficient Γ_s . The diagram of noise parameter measuring system is shown in Fig. 2. Various values of Γ_s have been realized using offset shorts and a 50-ohm termination. Noise contribution of test fixture and measurement setup including the mismatch effect between the device under test

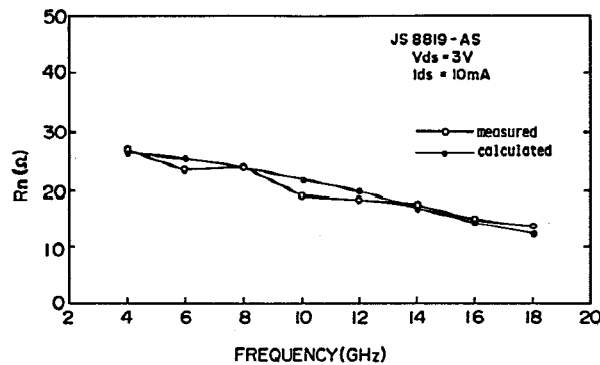
(DUT) and measuring system has been compensated for using the noise wave concept. This allows to eliminate the use of output tuner, thereby simplifying broadband noise parameter measurement. The DUTs have been mounted in a 50-ohm coplanar waveguide test fixture.

An example of measured noise parameters of Toshiba GaAs MESFET JS8819-AS is shown in Fig. 3, where the drain-source voltage $V_{ds} = 3$ V and drain current $I_d = 10$ mA.

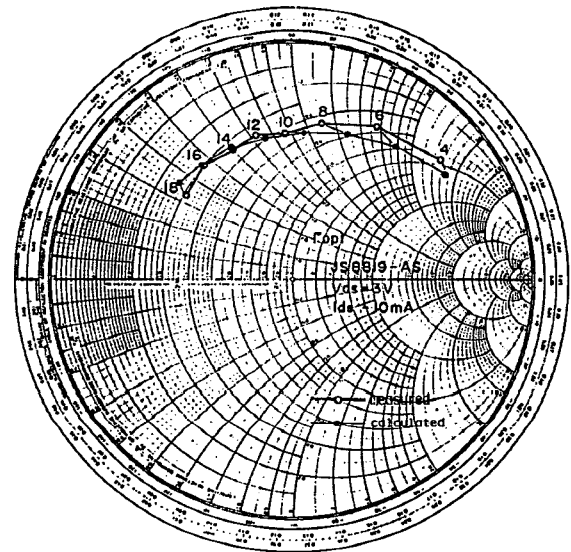
The small-signal equivalent circuit has been determined from S-parameters and DC measurements. The S-parameters have been measured over the frequency range of from 2 GHz to 18 GHz with an automatic network analyzer. In order to obtain the accurate value of parasitic resistances R_g , R_s and R_d , which generate thermal noise, the DC measurements have been done [13]. The equivalent circuit parameters have been determined by optimum fitting of the calculated S-parameters to the measured data.



(a)



(b)



(c)

Fig. 3 Frequency dependence of the measured and calculated noise parameters of a GaAs MESFET JS8819-AS. (a) Minimum noise figure F_{min} ; (b) Effective noise resistance R_n ; (c) Optimum source reflection coefficient Γ_s .

Experimental Results

Using the measured noise parameters and the small-signal equivalent circuit parameters, intrinsic noise parameters, G_{gn} , G_{dn} and C have been obtained by fitting the calculated results by Fig. 1 to the measured data. G_{dn} and C have been found to depend strongly upon the drain current I_d and gate width W_g , and have little dependence on the gate length for GaAs MESFETs with 0.25-0.5 μm . It is also found that G_{dn} per unit gate width (G_{dn}/W_g) and C are nearly determined by the drain current per unit gate width (I_d/W_g). On the other hand, G_{gn} has been found nearly equal to the input conductance of FETs. Thus we have

$$G_{gn} = R_i \omega^2 C_{gs}^2 / (1 + \omega^2 C_{gs}^2 R_i^2) \quad (5)$$

where ω denotes the radian frequency.

The measured I_d/W_g dependences of G_{dn}/W_g and C are shown in Fig. 4 and Fig. 5, respectively, where $V_{ds} = 3$ V, ambient temperature $T_0 = 298$ K and G_{gn} is given by eq. (5). The measurements have been done on Toshiba GaAs MESFETs of JS8819-AS, JS8818-AS, JS8830-AS and JS8870-AS, with a gate length of 0.5 μm and a gate width of 300 μm , 0.3 μm and 300 μm , 0.25 μm and 200 μm , and 0.5 μm and 300 μm , respectively. JS8870-AS is fabricated on ion-implanted wafers, and others on epi-wafers. From Fig. 4 and 5, the following experimental formulas have been obtained by least-square fitting;

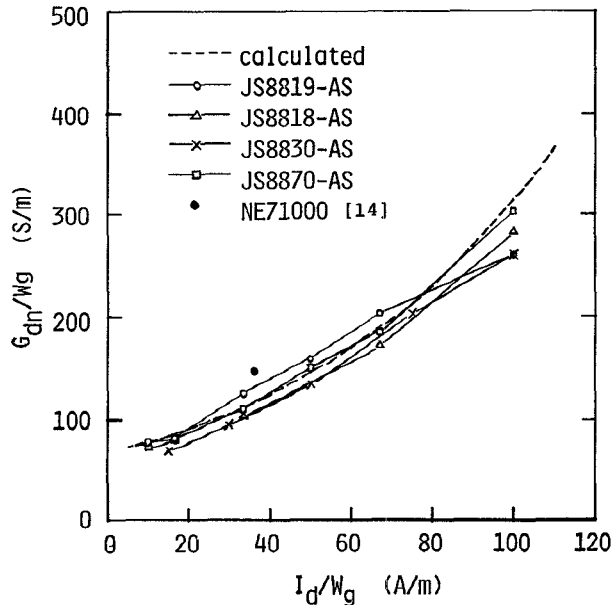


Fig. 4 I_d/W_g dependence of G_{dn}/W_g on various types of GaAs MESFETs at drain-source voltage of 3 V.

$$G_{dn} = 67.6 W_g \exp(0.0154 I_d/W_g) \quad (6)$$

$$C = 1.8 - 0.9 \exp(0.00245 I_d/W_g) \quad (7)$$

where G_{dn} is in S, I_d in A and W_g in m. In the figures, the calculated values from (6) and (7) are shown in broken lines. Furthermore an NEC GaAs MESFET NE71000 with 0.3 μm gate length and 280 μm gate width fabricated on epi-wafer also exhibits almost the same values as ours as plotted in Fig. 4 and 5. The data of NE71000 have been obtained from the noise parameters and S-parameters in technical data sheets [14]. These figures indicate that the formulas (5)-(7) give good approximations for the noise in intrinsic FETs.

The noise parameters of JS8819-AS calculated using (5)-(7) are shown in Fig. 3. The equivalent circuit element values of JS8819-AS at $V_{ds} = 3$ V and $I_d = 10$ mA are shown in Table 1. Fig. 6 shows the

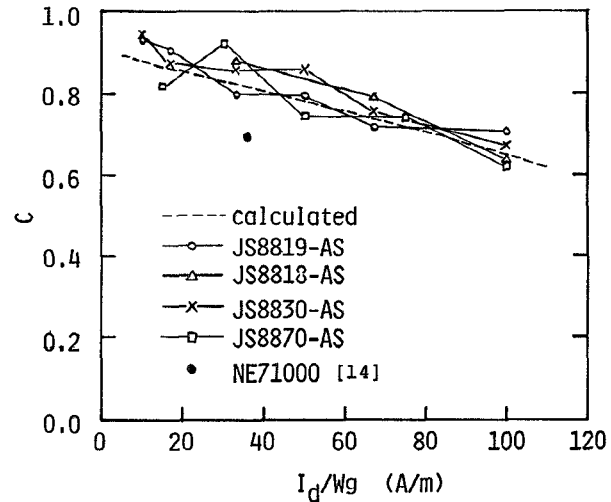


Fig. 5 I_d/W_g dependence of C on various types of GaAs MESFETs at drain-source voltage of 3 V.

Table 1 Equivalent circuit element values of JS8819-AS at $V_{ds} = 3$ V and $I_d = 10$ mA.

intrinsic elements	parasitic elements
$g_m = 44.7$ (mS)	$R_g = 3.32$ (Ω)
$\tau = 3.24$ (ps)	$R_s = 1.49$ (Ω)
$C_{gs} = 0.347$ (pF)	$R_d = 2.57$ (Ω)
$R_i = 2.78$ (Ω)	$C_{gd} = 0.034$ (pF)
$R_{ds} = 289$ (Ω)	$C_{ds} = 0.127$ (pF)
	$L_g = 0.119$ (nH)
	$L_s = 0.018$ (nH)
	$L_d = 0.077$ (nH)

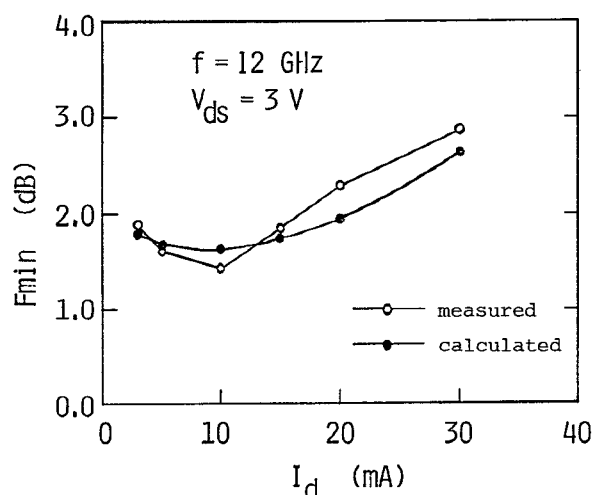


Fig. 6 I_d dependence of minimum noise figure F_{min} of JS8819-AS at a frequency of 12 GHz and V_{ds} of 3 V.

drain current dependence of the measured and calculated minimum noise figure F_{min} at a frequency of 12 GHz and $V_{ds} = 3$ V. As shown in Fig. 3 and Fig. 6, a good agreement is obtained between the model and measurement. This means that noise parameters are well characterized by using the formulas (5)-(7). Hence the model proposed here is suitable for efficient calculation of noise characteristics of GaAs MESFET.

Conclusion

A simple empirical noise model of GaAs MESFETs with submicron gate has been presented. The intrinsic noise current sources can be described by simple experimental formulas from the measured results on various types of GaAs MESFETs, and hence the noise parameters can be calculated without additional noise measurement. Thus the model gives an efficient means for computer-aided design of microwave integrated circuits in terms of noise optimum design.

Acknowledgment

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